

Suspensions of viscoelastic capsules: effect of membrane viscosity on transient dynamics

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Motivations: why viscoelastic capsules are important?

Biomedical applications

Pharmaceutical industry

Cosmetic

Food processing

- Designing some **biomedical devices** (e.g., heart pumps)
- **Reduced models** to estimate the **rate of hemolysis** that take the **mechanical properties** of red blood cells (RBCs) as input
- Characterise the **deformation** of RBCs and the **time** they take to **deform**

KEYWORDS

- # Viscoelastic membrane
- # Deformation
- # Deformation time

Effects of membrane viscosity μ_m on RBC dynamics

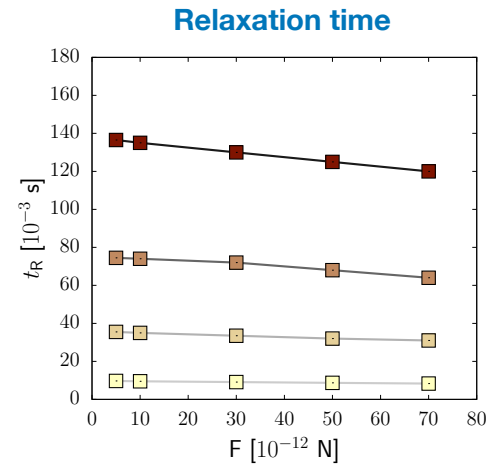
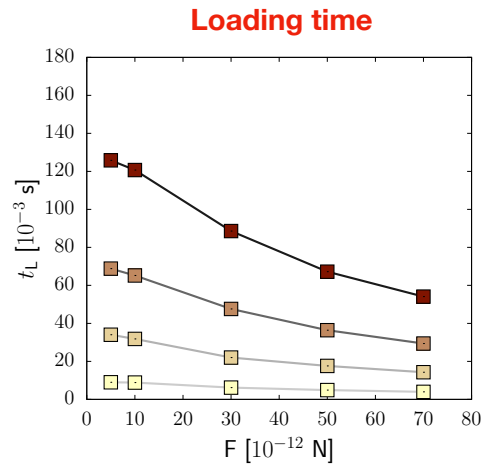
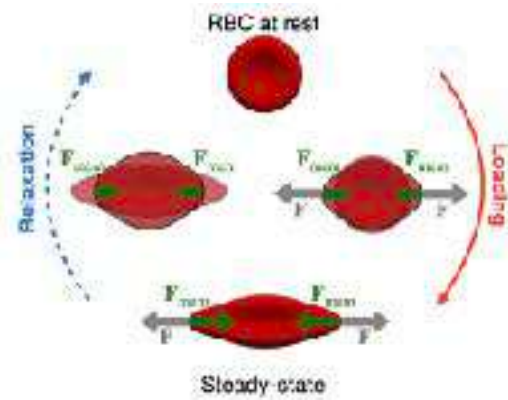
- Increasing μ_m results in an **increase of the loading time** t_L ^[1,2]
- Depending on the flow conditions even the steady value of the **deformation depends on** μ_m ^[1,2]



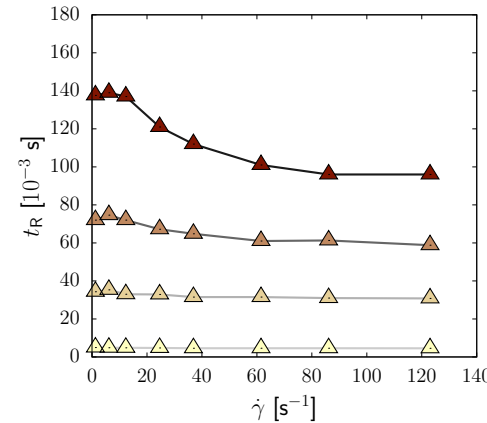
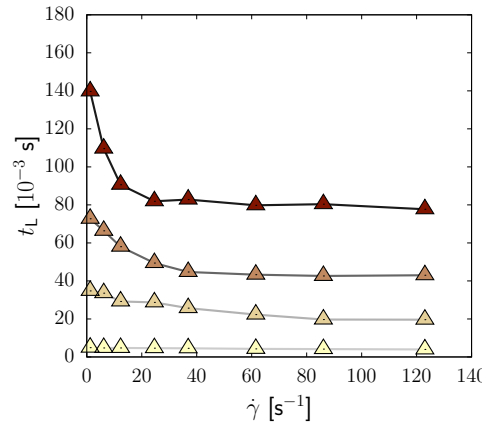
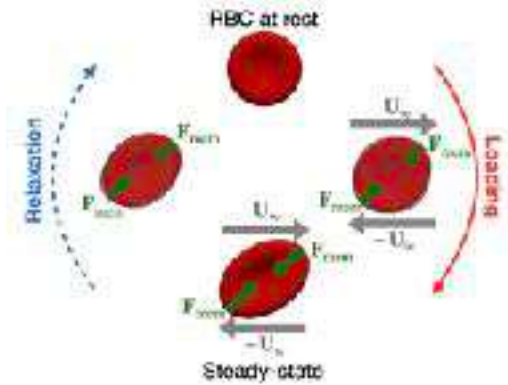
(1) **Guglietta, F.**, Behr, M., Biferale, L., Falcucci, G., & Sbragaglia, M. (2020). On the effects of membrane viscosity on transient red blood cell dynamics. *Soft Matter*, 16(26), 6191-6205.

(2) **Guglietta, F.**, Behr, M., Falcucci, G., & Sbragaglia, M. (2021). Loading and relaxation dynamics of a red blood cell. *Soft Matter*, 17(24), 5978-5990.

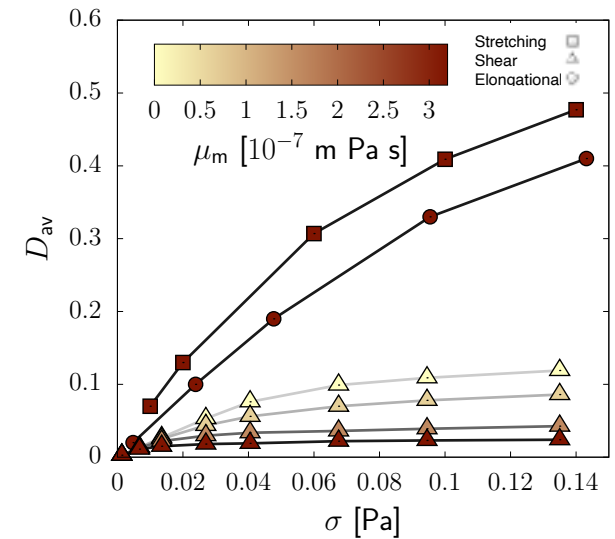
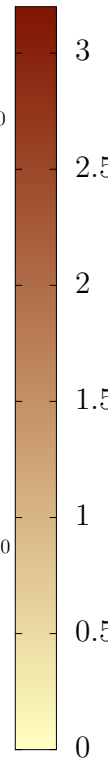
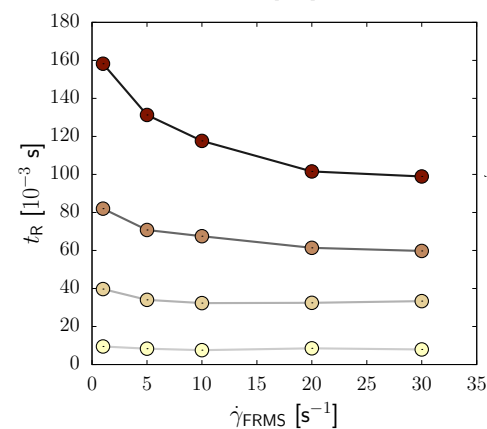
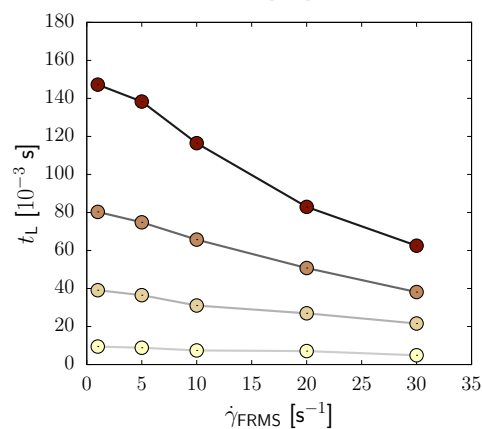
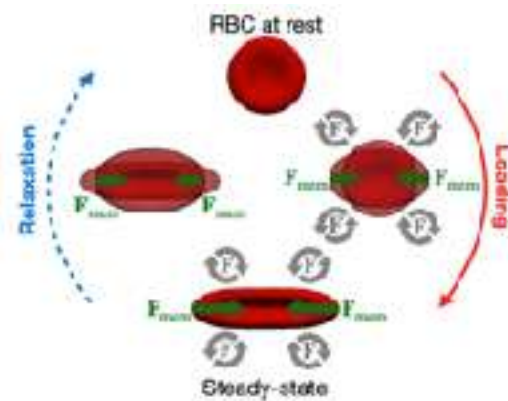
Stretching
with
optical
tweezers



Simple shear
flow

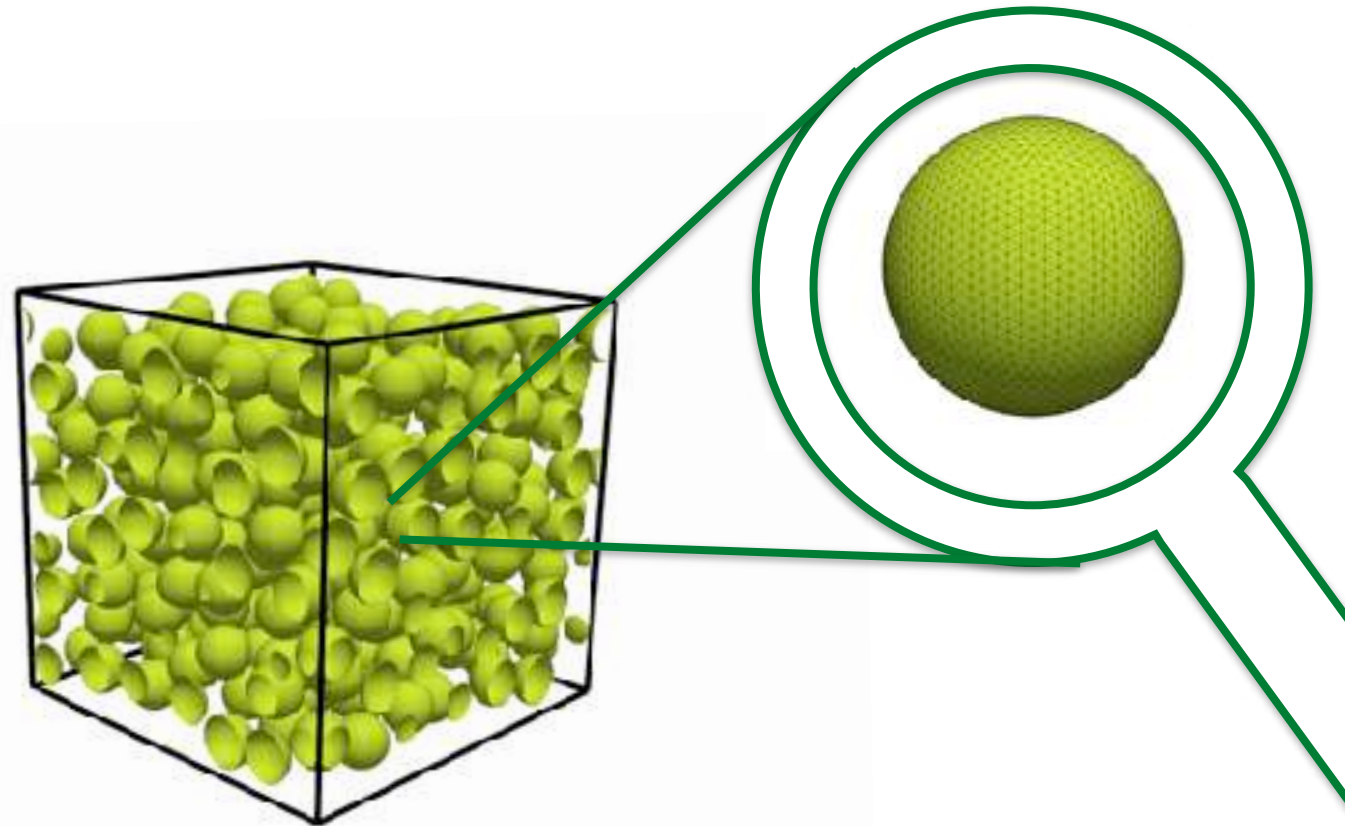


Elongational
flow



Guglietta, F., Behr, M., Falcucci, G., & Sbragaglia, M. (2021). Loading and relaxation dynamics of a red blood cell. *Soft Matter*, 17(24), 5978-5990.

- ▶ **Aim:** Characterise the effect of **membrane viscosity** on the mechanical response (i.e., deformation, loading time) of suspensions of viscoelastic spherical capsules.
- ▶ **Numerical model:**
 - ▶ Viscoelastic **membrane** model
 - ▶ **Fluid** solver
- ▶ **Results:**
 - ▶ **Single** viscoelastic capsule
 - ▶ **Suspensions** of viscoelastic capsules





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Numerical model

Energy:
 $W = W_s + W_v$

Skalak model (resistance against strain) [1,2]

$$W_s = \frac{1}{12} \int \left[\underset{\substack{\uparrow \\ \text{Elastic shear modulus}}}{k_s} (I_1^2 + 2I_1 - 2I_2) + \underset{\substack{\uparrow \\ \text{Elastic dilatational modulus}}}{k_\alpha} I_2^2 \right] dS$$

Strain invariants: $I_1 = \lambda_x^2 + \lambda_y^2 - 2$ λ_x and λ_y are the principal stretch ratios
 $I_2 = \lambda_x^2 \lambda_y^2 - 1$

Global volume conservation [2]

$$W_v = \frac{k_v}{2} \frac{(V - V_0)^2}{V_0}$$

Volume modulus: k_v

Initial volume: V_0

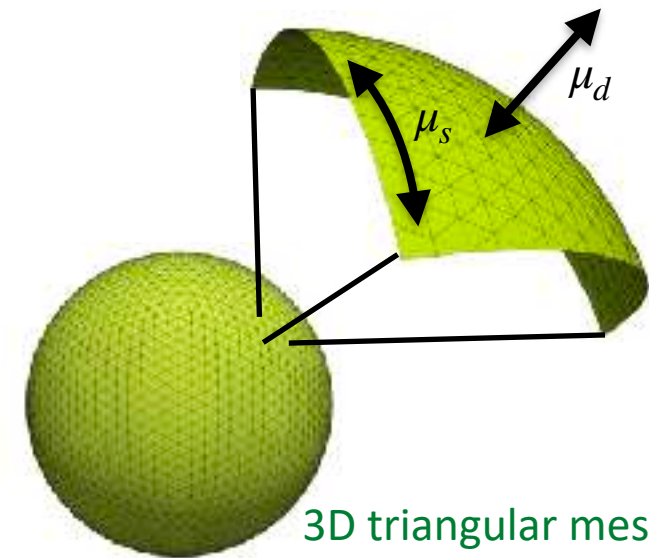
Viscous tensor:
 τ^v

Boussinesq-Scriven law [3,4]

$$\tau^v = \underset{\substack{\uparrow \\ \text{Shear membrane viscosity}}}{\mu_s} [2\mathbf{E} - \text{tr}(\mathbf{E})\mathbf{I}] + \underset{\substack{\uparrow \\ \text{Dilatational membrane viscosity}}}{\mu_d} \text{tr}(\mathbf{E})\mathbf{I} = 2\underset{\substack{\uparrow \\ \text{Membrane viscosity}}}{\mu_m} \mathbf{E}$$

$\mathbf{E} = \frac{1}{2}[\nabla \mathbf{u} + \nabla \mathbf{u}^T]$

Repulsive force [5]: $\vec{\varphi}_{ij} = \begin{cases} \bar{e} \left[\left(\frac{\Delta x}{d_{ij}} \right)^2 - \left(\frac{\Delta x}{\delta_0} \right)^2 \right] \hat{d}_{ij} & \text{if } d_{ij} < \delta_0, \\ 0 & \text{if } d_{ij} \geq \delta_0, \end{cases}$



3D triangular mesh
(5120 faces)

(1) Skalak, R., Tozeren, A., Zarda, R. P., & Chien, S. (1973). Strain energy function of red blood cell membranes. *Biophysical journal*, 13(3), 245-264.
 (2) Krüger, T. (2012). Computer simulation study of collective phenomena in dense suspensions of red blood cells under shear. Springer Science & Business Media.
 (3) Barthès-Biesel, D., & Sgaier, H. (1985). Role of membrane viscosity in the orientation and deformation of a spherical capsule suspended in shear flow. *Journal of Fluid Mechanics*, 160, 119-135.
 (4) Li, P., & Zhang, J. (2019). A finite difference method with subsampling for immersed boundary simulations of the capsule dynamics with viscoelastic membranes. *Int. J. Numer. Methods Biomed. Eng.*, 35(6), e3200.
 (5) Aouane, O., Scagliarini, A., & Harting, J. (2021). Structure and rheology of suspensions of spherical strain-hardening capsules. *Journal of Fluid Mechanics*, 911.

Immersed boundary - lattice Boltzmann (IB-LB) method

Lattice Boltzmann (LB) method [1]

$$f_i(\mathbf{x} + \mathbf{c}_i \Delta t, t + \Delta t) - f_i(\mathbf{x}, t) = \Delta t \left[\overset{\text{Collision}}{\Omega_i(\mathbf{x}, t)} + \left(1 - \frac{1}{2\tau}\right) \overset{\text{Membrane forces}}{F_i(\mathbf{x}, t)} \right]$$

$\xrightarrow{\text{Streaming}}$
 $\xrightarrow{\text{Collision}}$
 $\xrightarrow{\text{Membrane forces}}$

Populations: $f_i(\mathbf{x}, t)$

Density of mass in the physical space and in the (kinetic) velocity space

Fluid density

$$\rho(\mathbf{x}, t) = \sum_i f_i(\mathbf{x}, t)$$

Fluid velocity

$$\rho \mathbf{u}(\mathbf{x}, t) = \sum_i \mathbf{c}_i f_i(\mathbf{x}, t)$$

Immersed boundary (IB) method [1]

membrane → **fluid**

$$\mathbf{F}(\mathbf{x}, t) = \sum_j \varphi_j(t) \Delta(\mathbf{r}_j(t), \mathbf{x}) + \mathbf{F}_{other}$$

fluid → **membrane**

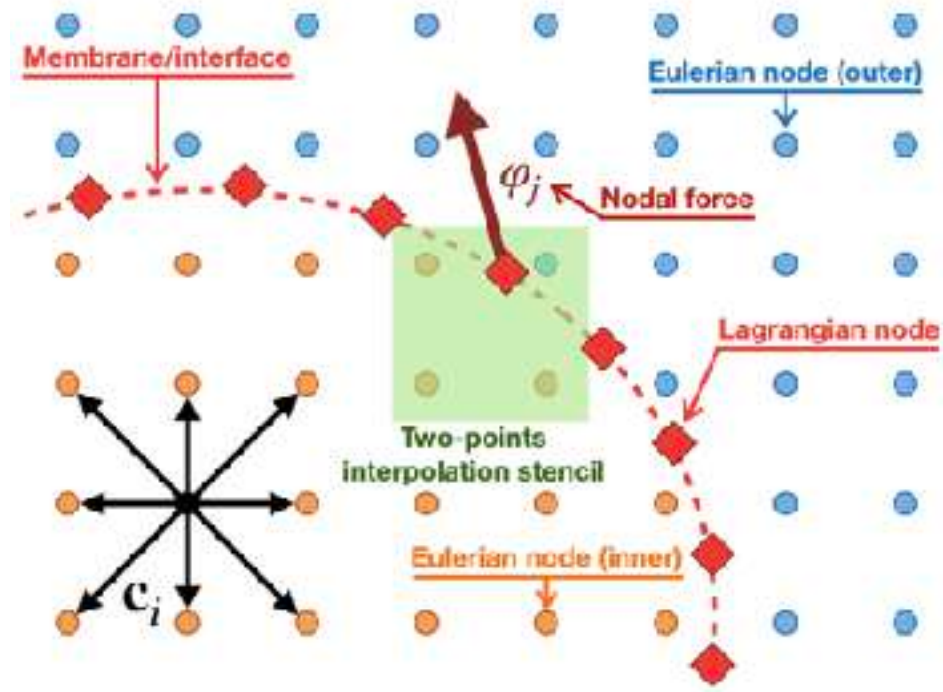
$$\dot{\mathbf{r}}_j(t) = \sum_{\mathbf{x}} \Delta x^3 \mathbf{u}(\mathbf{x}, t) \Delta(\mathbf{r}_j(t), \mathbf{x})$$

$$\mathbf{r}_j(t + \Delta t) = \mathbf{r}_j(t) + \dot{\mathbf{r}}_j(t)$$

Discrete Dirac delta

$$\Delta(\mathbf{x}) = \frac{\Phi(x)\Phi(y)\Phi(z)}{\Delta x^3}$$

$$\Phi_2(x) = \begin{cases} 1 - |x| & 0 \leq |x| \leq \Delta x \\ 0 & \Delta x \leq |x| \end{cases}$$



(1) Krüger, T., Kusumaatmaja, H., Kuzmin, A., Shardt, O., Silva, G., & Vigen, E. M. (2017). The lattice Boltzmann method. Springer International Publishing, 10(978-3), 4-15.



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Results: single capsule

Single capsule in simple shear flow

Reynolds number:

$$Re = \frac{\dot{\gamma} \rho r^2}{\mu} = 10^{-2}$$

Capillary number:

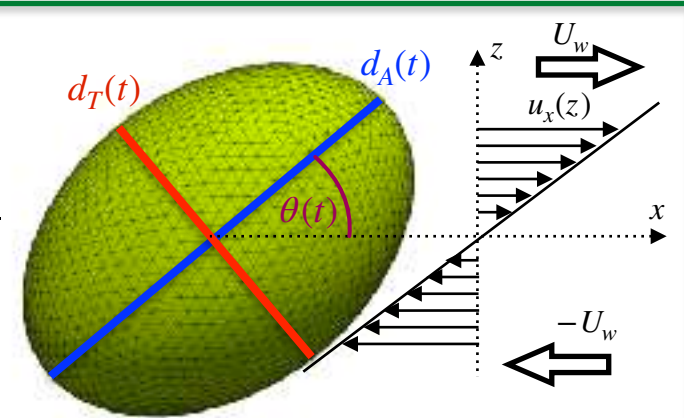
$$Ca = \frac{\dot{\gamma} \mu r}{k_s} = \dot{\gamma} t^* \in [0.1, 1]$$

Boussinesq number:

$$Bq = \frac{\mu_m}{\mu r} \in [0, 50]$$

Radius: r
 Shear rate: $\dot{\gamma}$
 Fluid viscosity: μ
 Membrane viscosity: μ_m
 Intrinsic time: $t^* = \mu r / k_s$

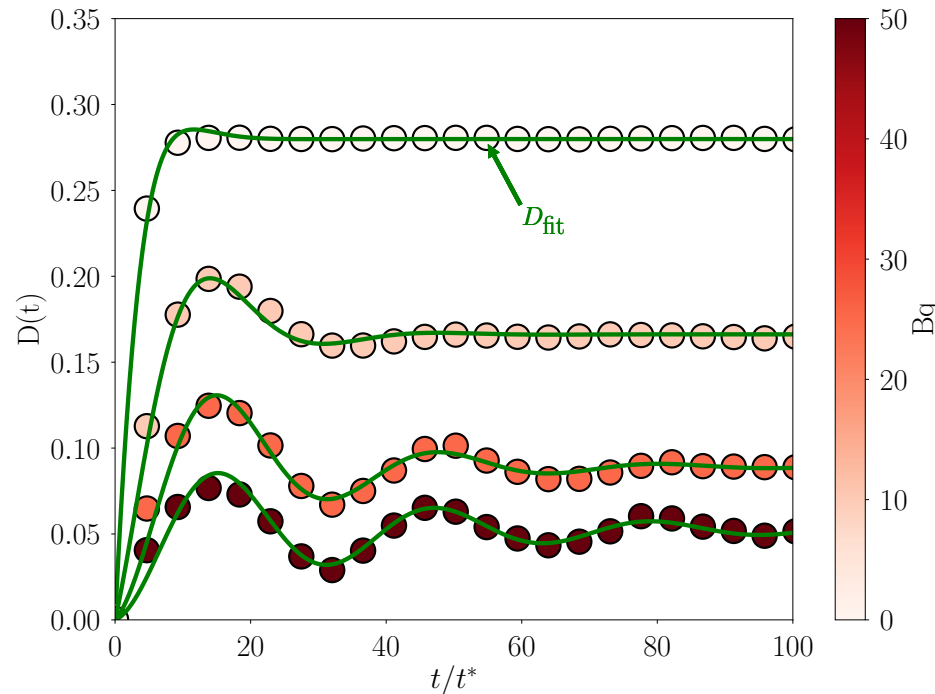
$$D(t) = \frac{d_A(t) - d_T(t)}{d_A(t) + d_T(t)}$$



Fit function:

$$D_{\text{fit}}\left(\frac{t}{t^*}\right) = \bar{D} \left[1 - \exp\left(-\frac{t}{t^* t_L}\right) \cos\left(\omega \frac{t}{t^*}\right) \right]$$

Fit parameters: t_L, ω



$Bq = 0$



$Bq = 50$





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Results: suspensions of capsule

Suspension of viscoelastic capsules

Reynolds number: $Re = \frac{\dot{\gamma} \rho r^2}{\mu} = 10^{-2}$

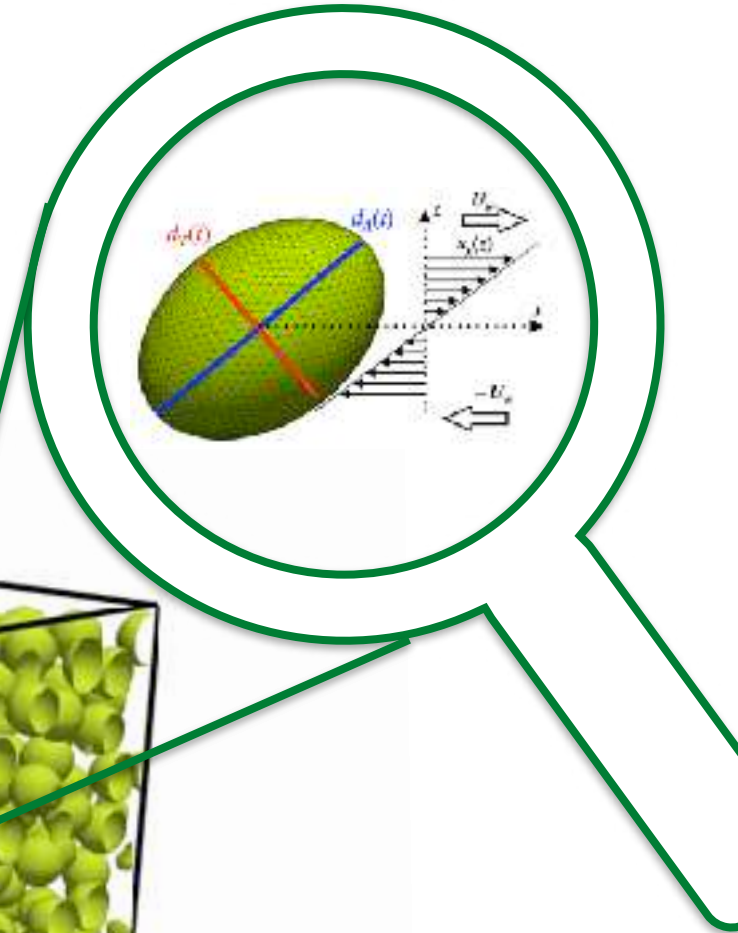
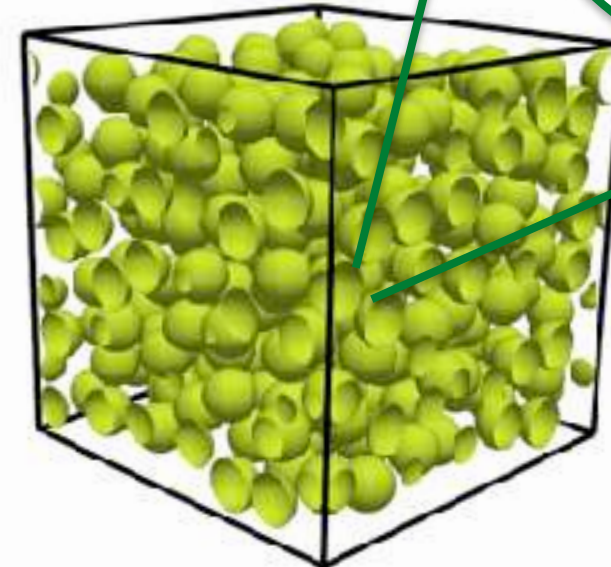
Capillary number: $Ca = \frac{\dot{\gamma} \mu r}{k_s} = \dot{\gamma} t^* \in [0.1, 1]$

Boussinesq number: $Bq = \frac{\mu_m}{\mu r} \in [0, 50]$

Volume fraction: $\phi = \frac{\sum_i V_i}{L^3} \in [0.001, 0.4]$

Deformation: $\langle D \rangle = \frac{1}{N} \sum_i D_i(t)$

Radius: r
Shear rate: $\dot{\gamma}$
Fluid viscosity: μ
Capsule Volume: V_i
Membrane viscosity: μ_m
Intrinsic time: $t^* = \mu r / k_s$



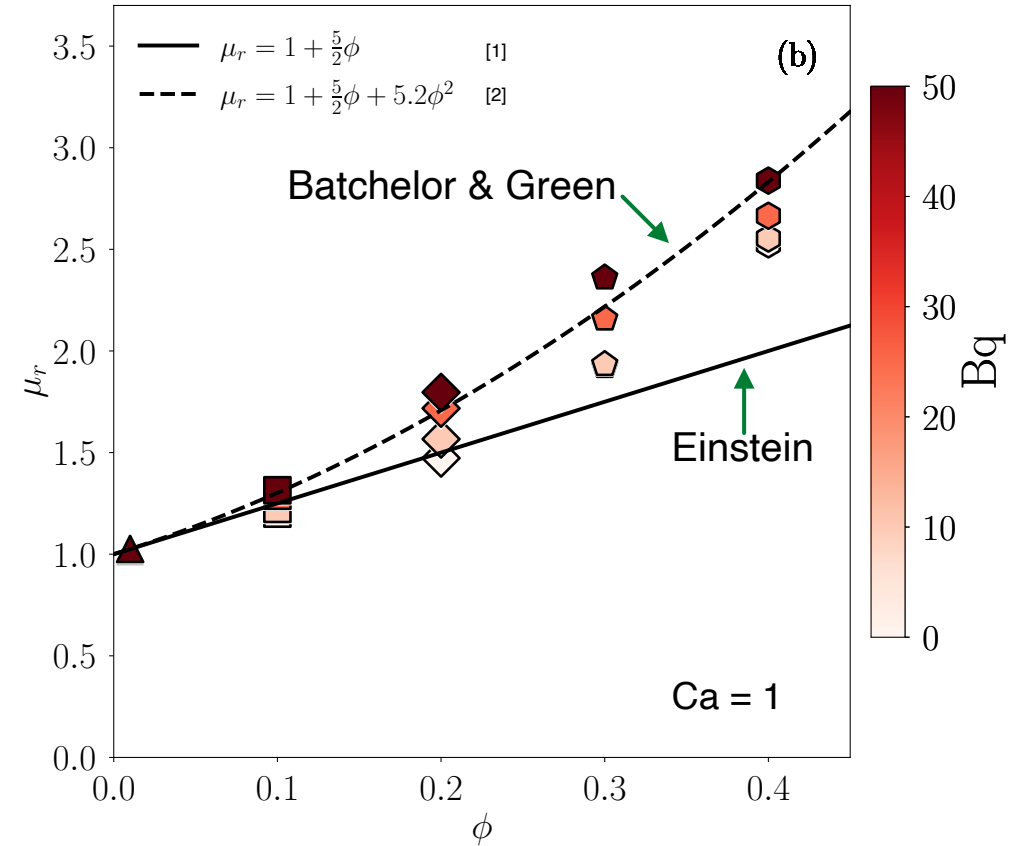
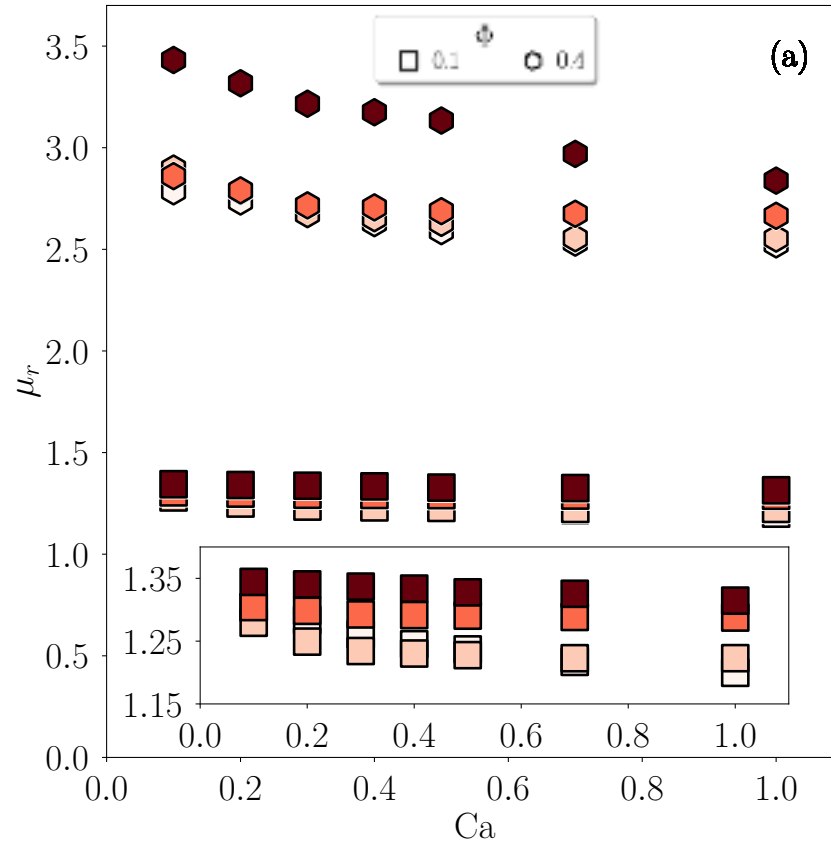
Rheology: relative viscosity

Suspension viscosity \downarrow Particle stress \downarrow

$$\mu_r = \frac{\mu_s}{\mu} = 1 + \frac{\sum p_{xz}^p}{\dot{\gamma}\mu}$$

$$Ca = \frac{\mu\dot{\gamma}R}{k_s}$$

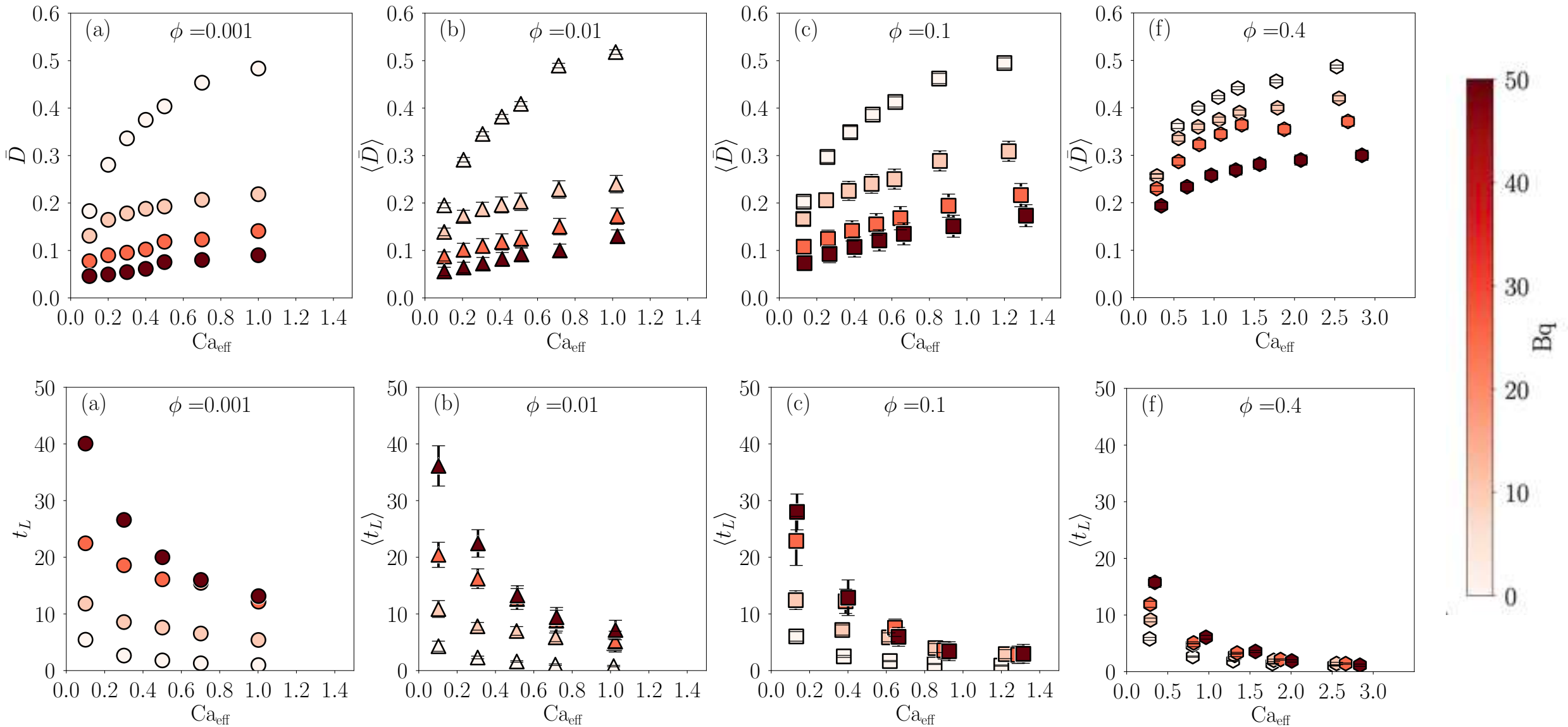
$$Ca_{\text{eff}} = \frac{\mu_s\dot{\gamma}R}{k_s} = Ca\mu_r$$



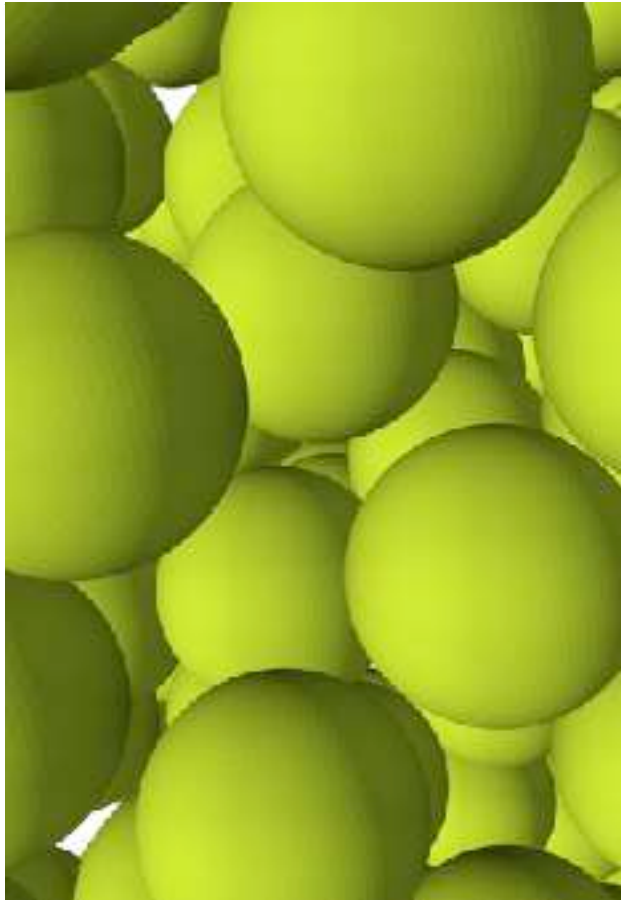
[1] Einstein, A. (1905). *Eine neue bestimmung der moleküldimensionen* (Doctoral dissertation).

[2] Batchelor, G. K., & Green, J. (1972). The determination of the bulk stress in a suspension of spherical particles to order c^2 . *Journal of Fluid Mechanics*, 56(3), 401-427.

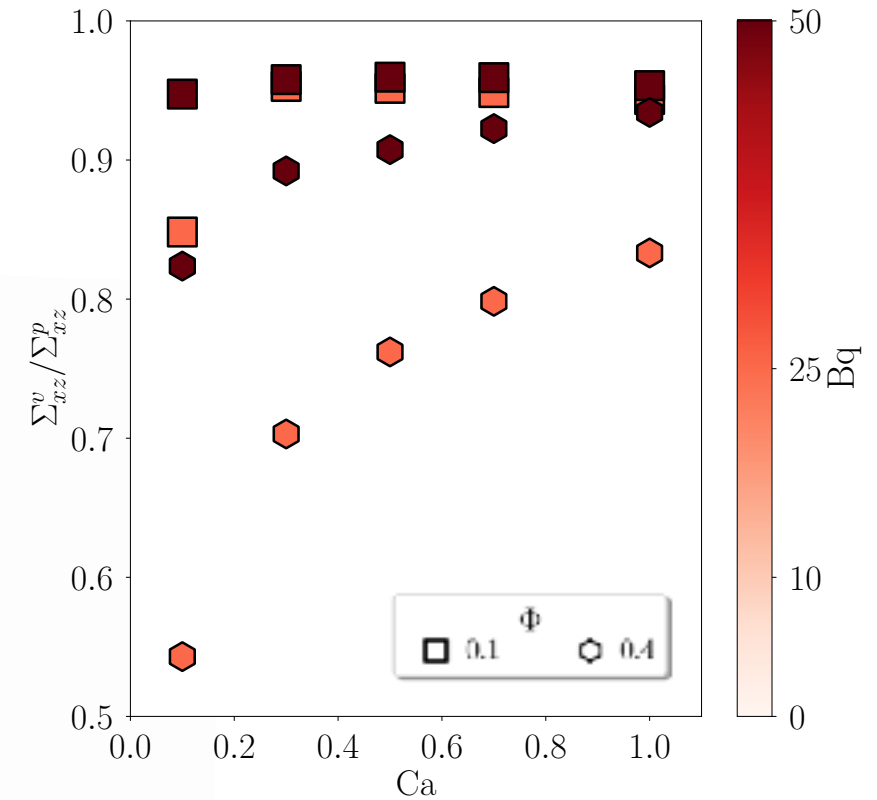
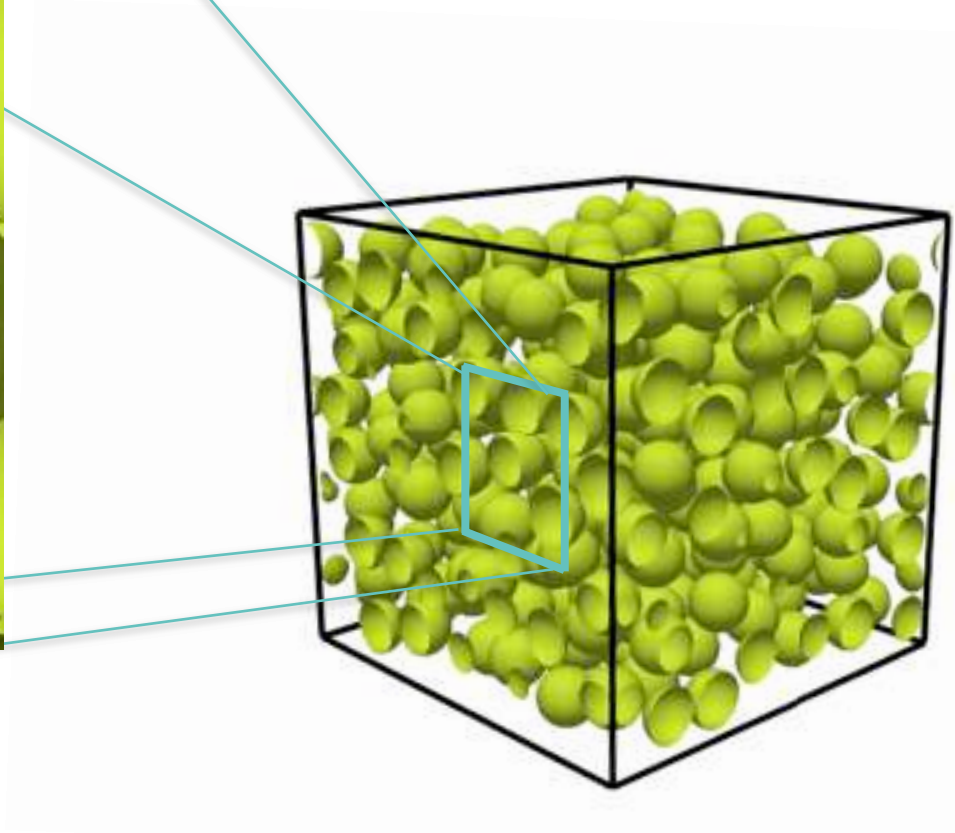
Deformation and inclination angle



Membrane viscosity and volume fraction



Boussinesq-Scriven law
$$\tau^v = 2\mu_m \mathbf{E} = \mu_m [\nabla \mathbf{u} + \nabla \mathbf{u}^T]$$



When the **volume fraction increases**, the **viscous dissipation reduces**

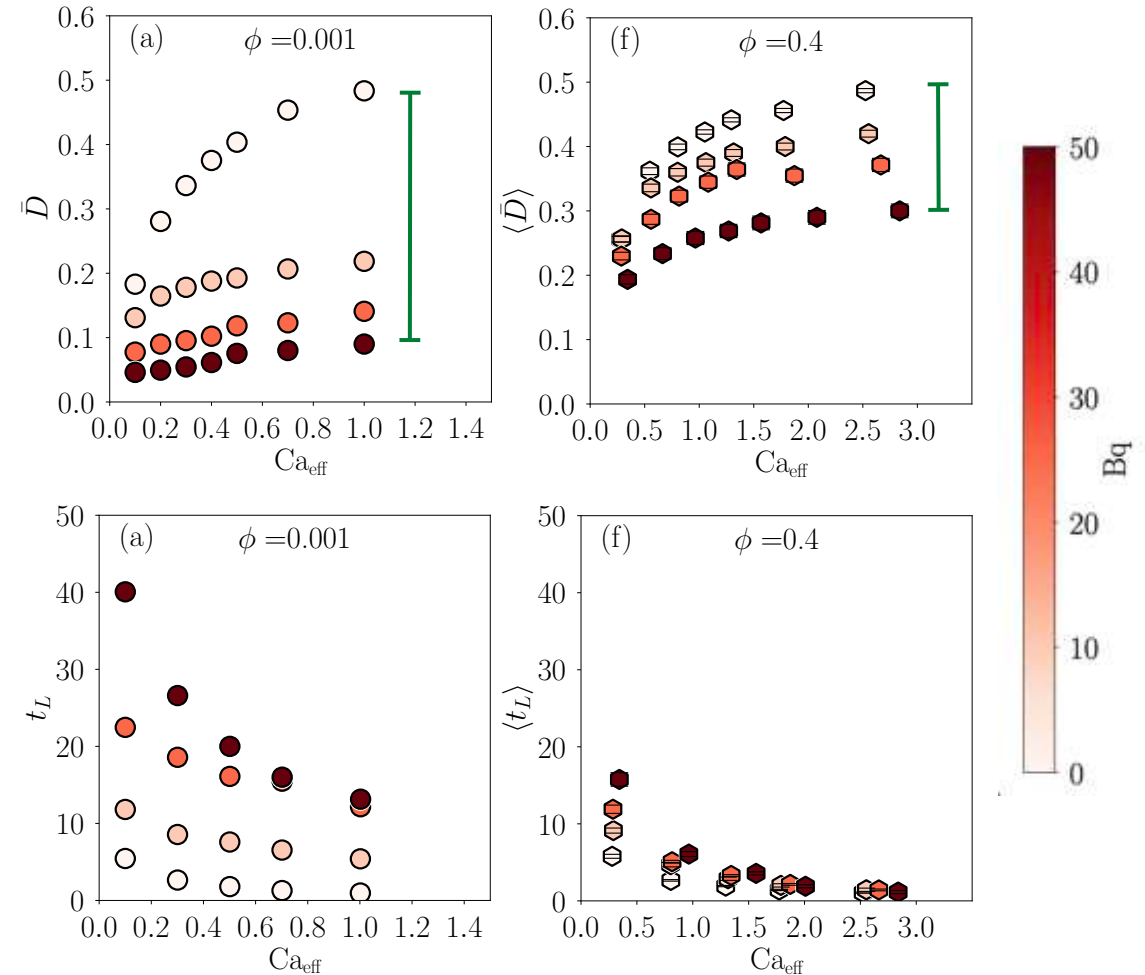
What's the effect of membrane viscosity?

► For a **fixed value of ϕ** , the effect of Bq is to:

- reduce the deformation
- increase the loading time

► When ϕ **increases**:

- the effect of Bq on D reduces
- the effect of Bq on t_L almost vanishes



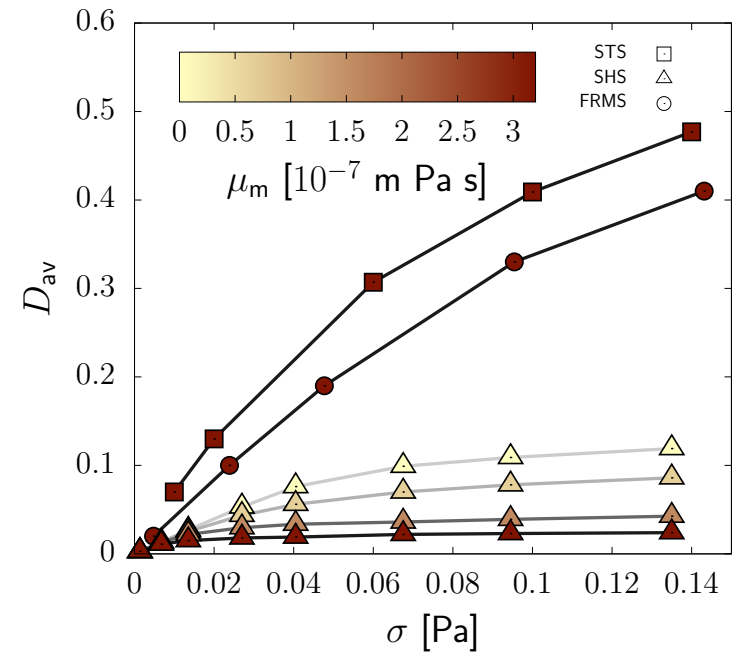
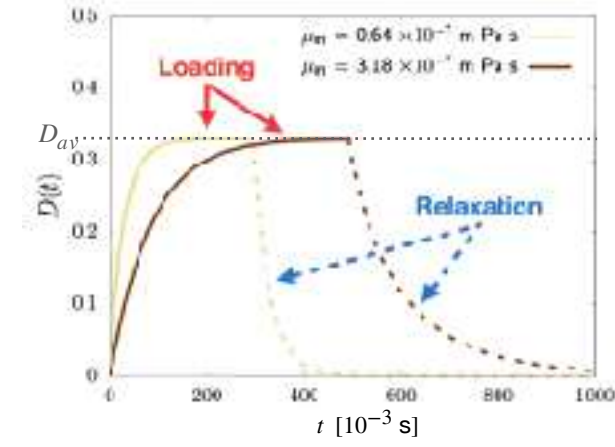
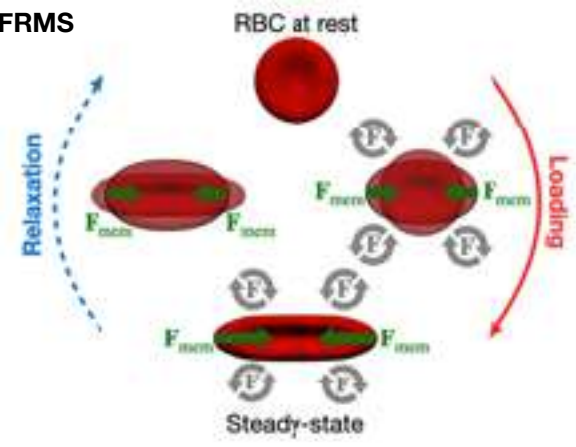
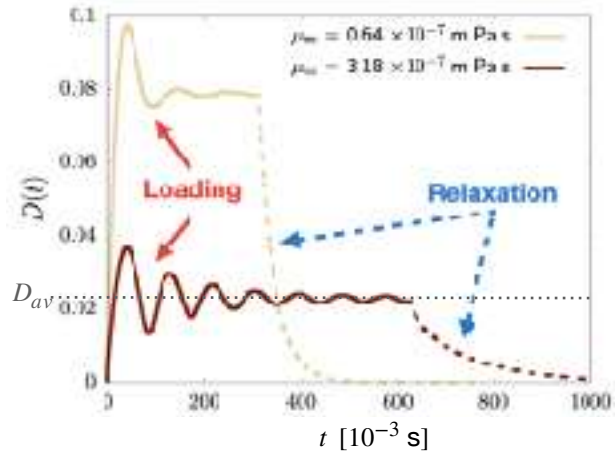
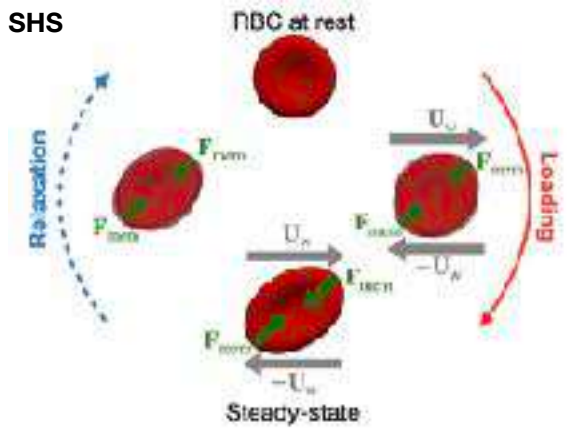
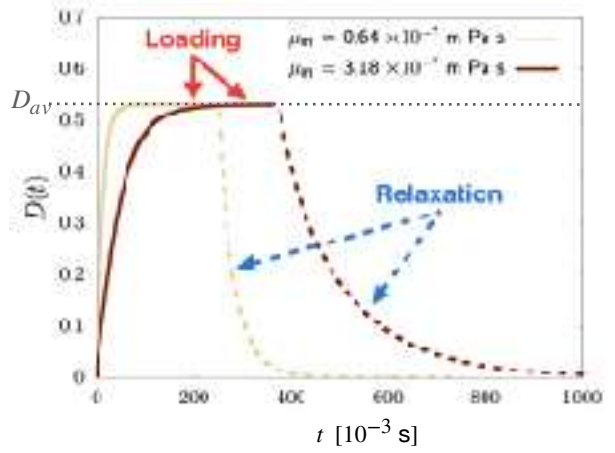
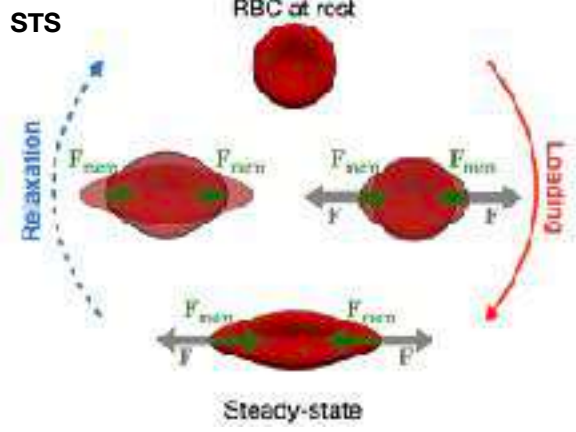
This work was supported by the Italian Ministry of University and Research (MUR) under the FARE programme, project “Smart-HEART”

Thank you!



Guglietta, F., Pelusi, F., Segal, M., Aouane, O., & Harting, J. (2023).
Suspensions of viscoelastic capsules: Effect of membrane viscosity on transient dynamics.
Journal of Fluid Mechanics, **971**, A13. doi:10.1017/jfm.2023.694

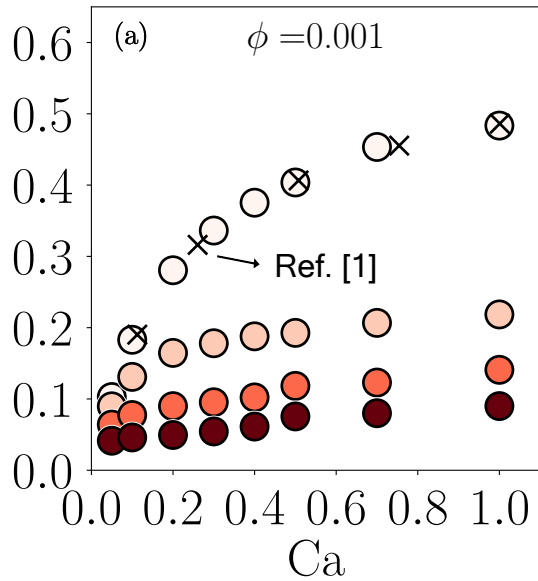
BACKUP SLIDES



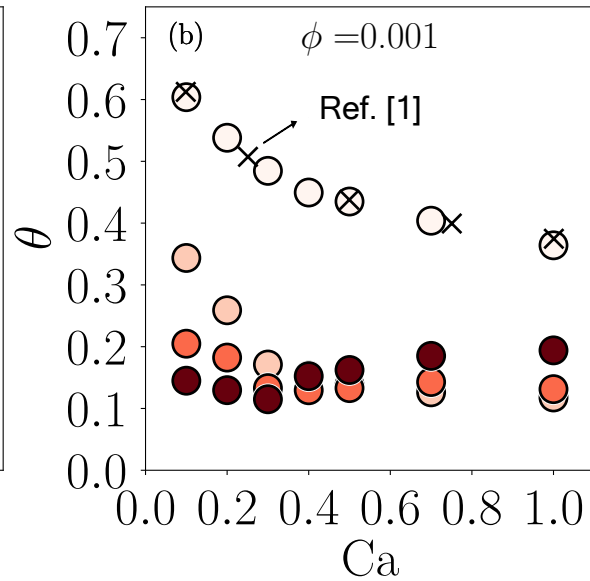
- **The steady value of deformation** may depend on the value of **membrane viscosity**
- **The rotation of the membrane dissipates** part of the energy otherwise used to **deform** the membrane.

Single capsule in simple shear flow

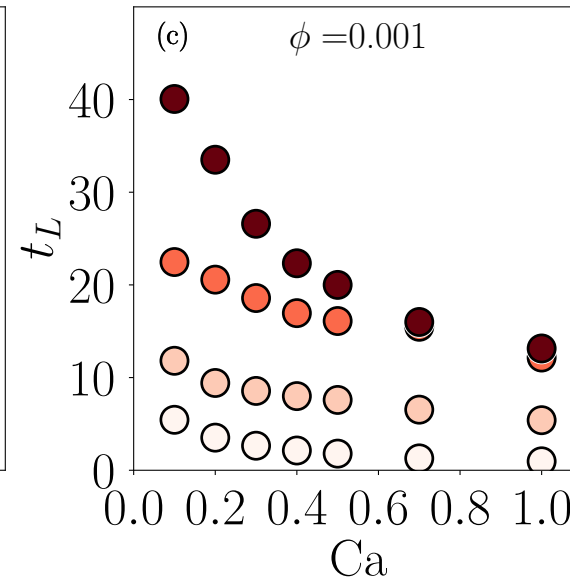
Deformation



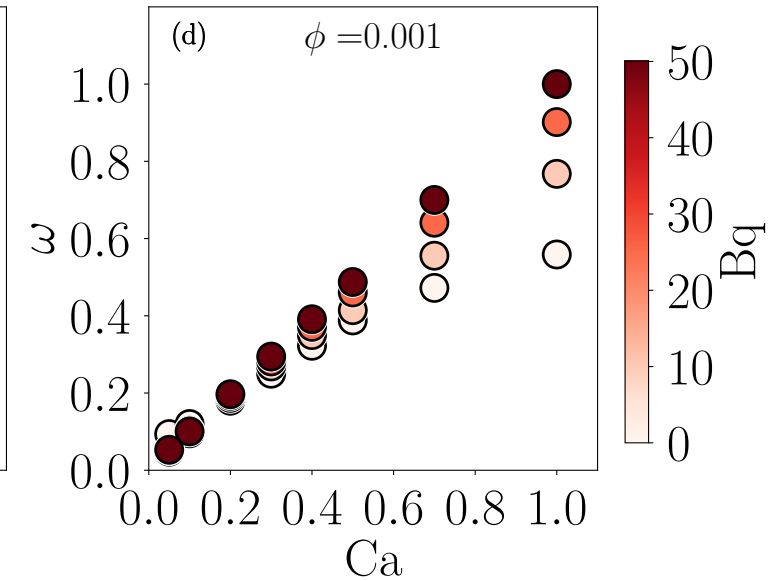
Inclination angle



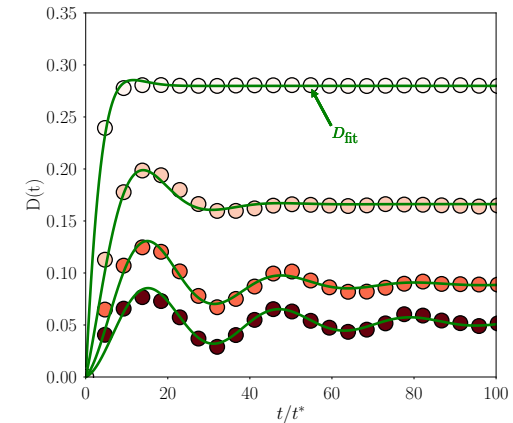
Loading time



Frequency

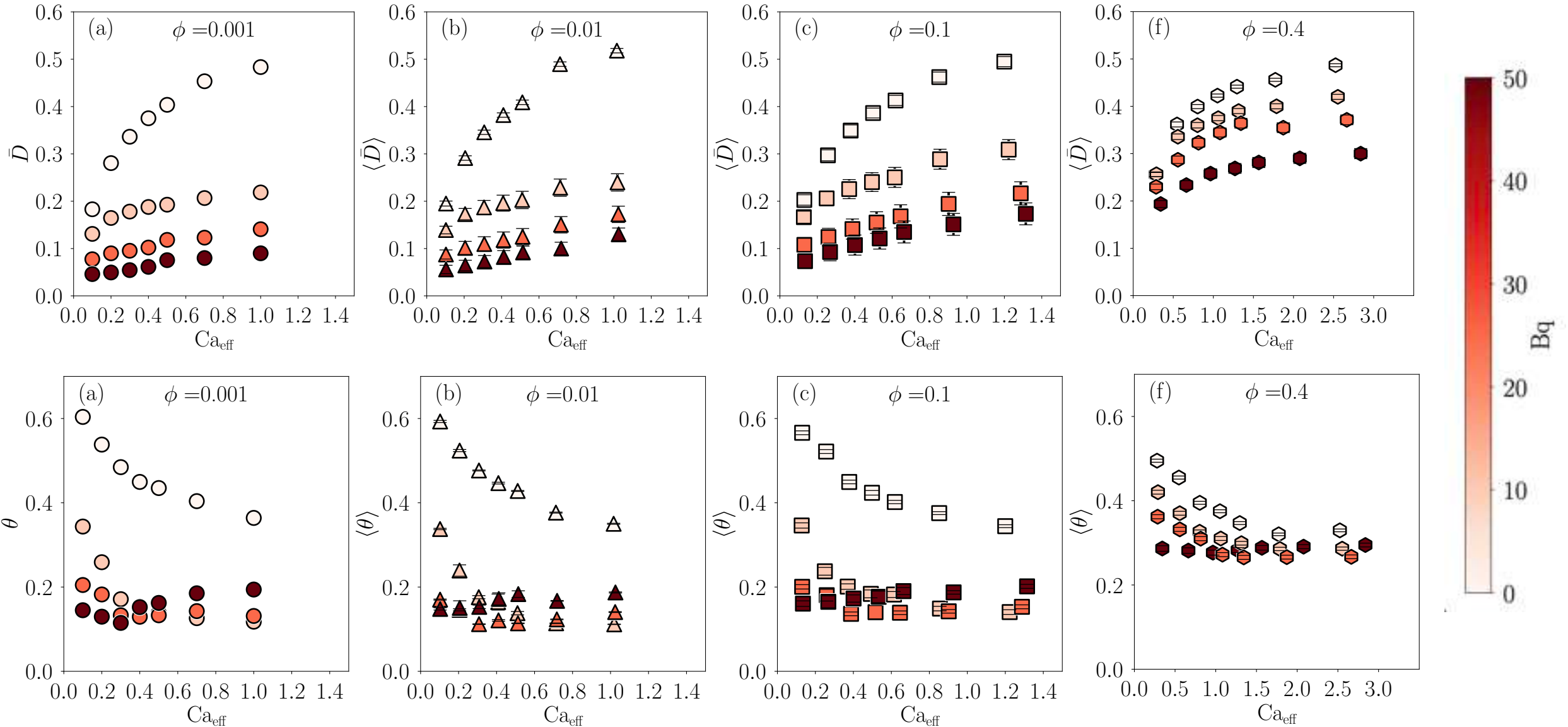


$$D_{\text{fit}}\left(\frac{t}{t^*}\right) = \bar{D} \left[1 - \exp\left(-\frac{t}{t^* t_L}\right) \cos\left(\omega \frac{t}{t^*}\right) \right]$$

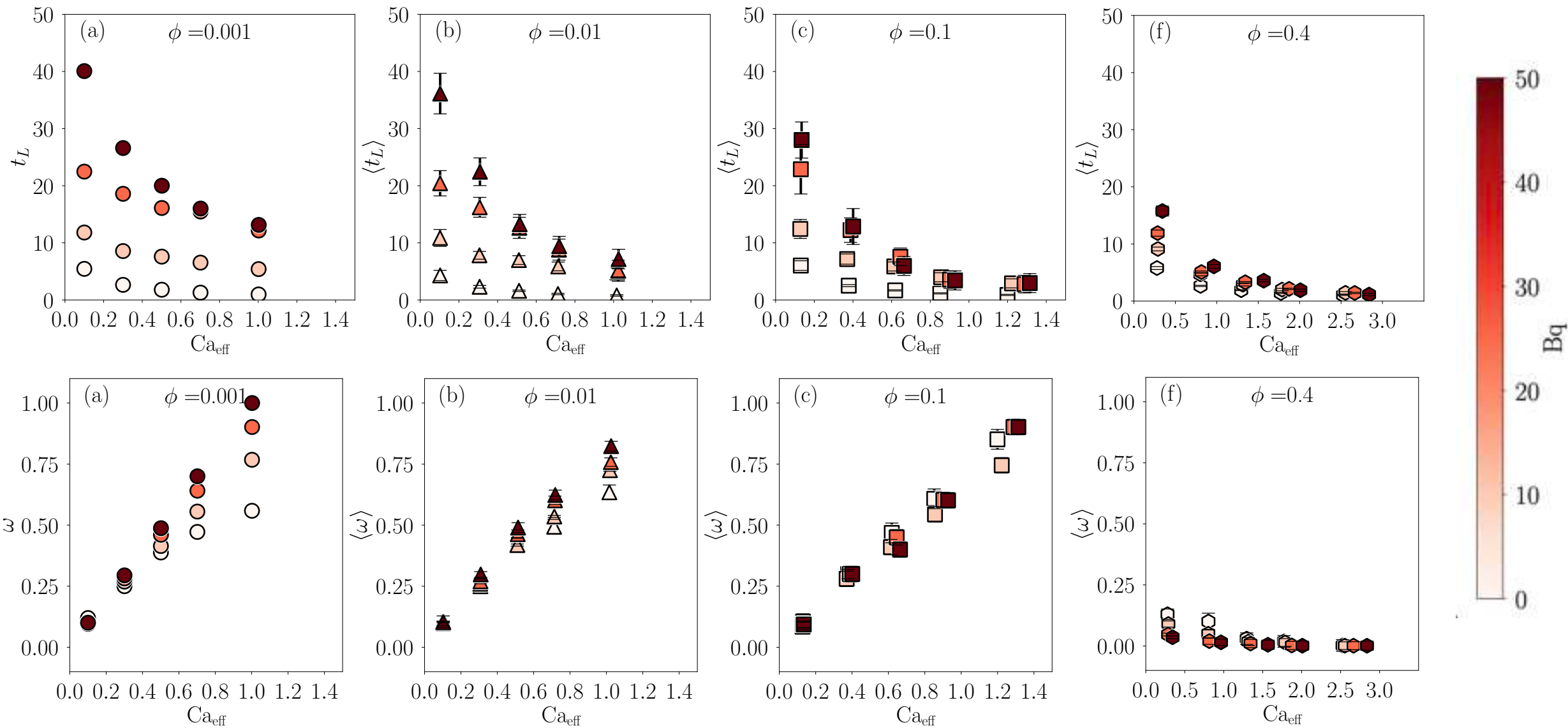


(1) Aouane, O., Scagliarini, A., & Harting, J. (2021). Structure and rheology of suspensions of spherical strain-hardening capsules. Journal of Fluid Mechanics, 911.

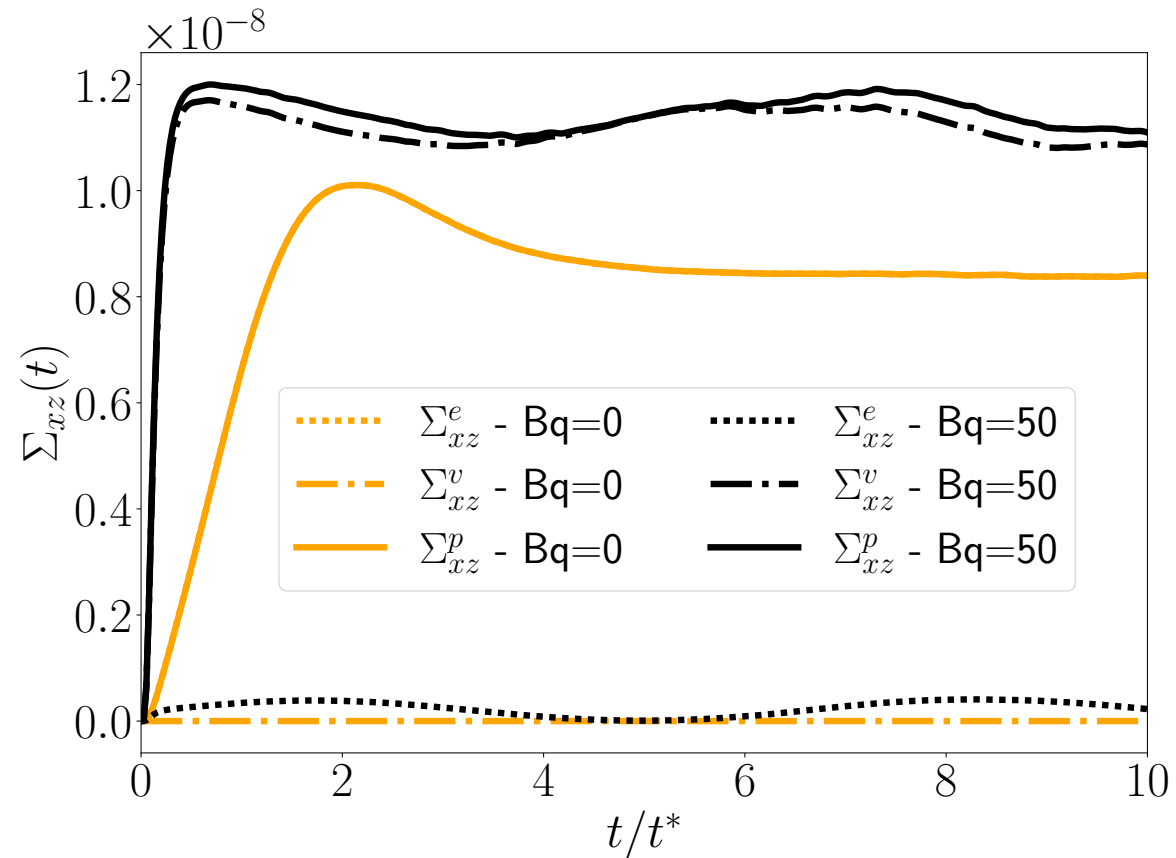
Deformation and inclination angle

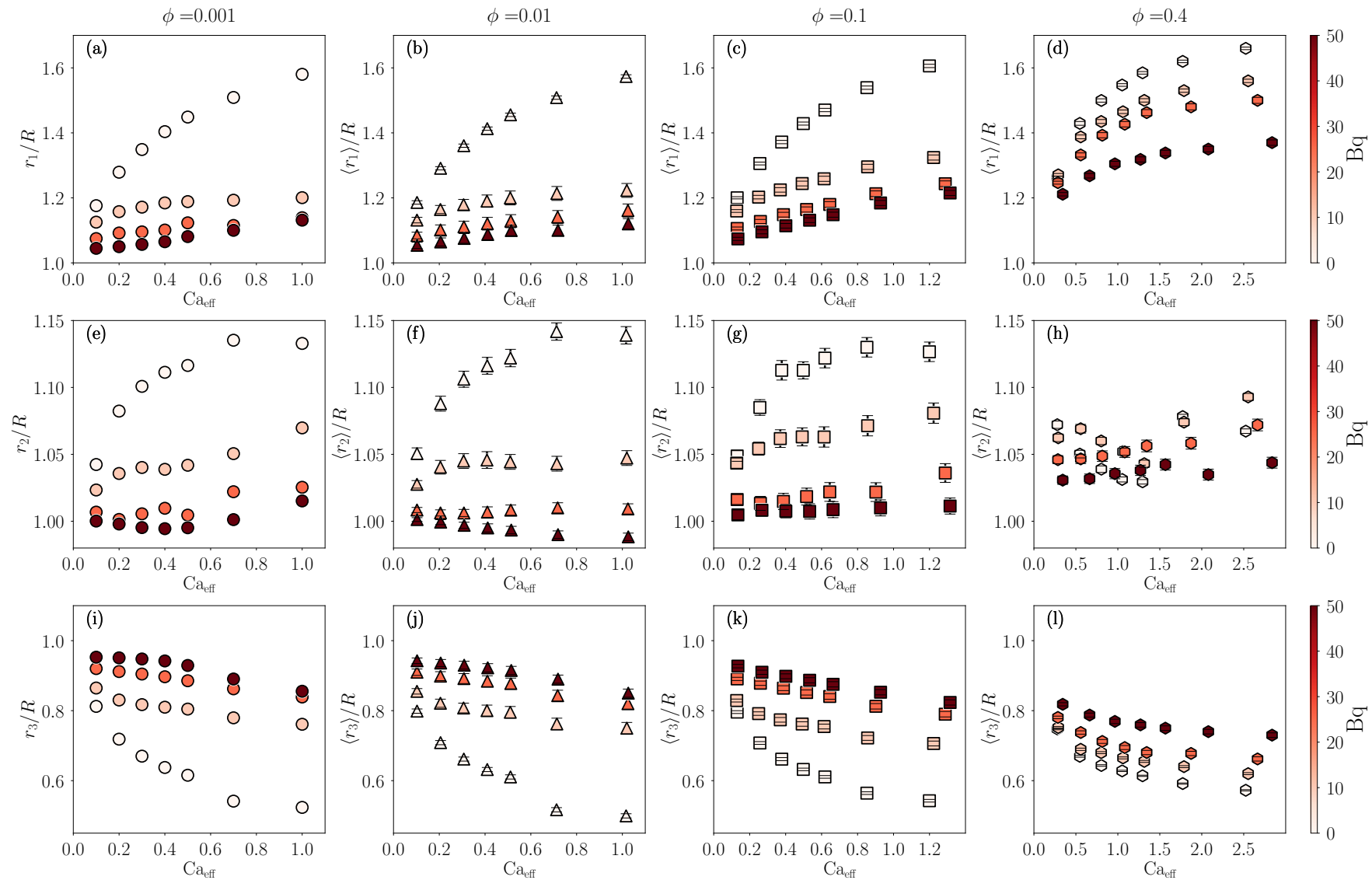


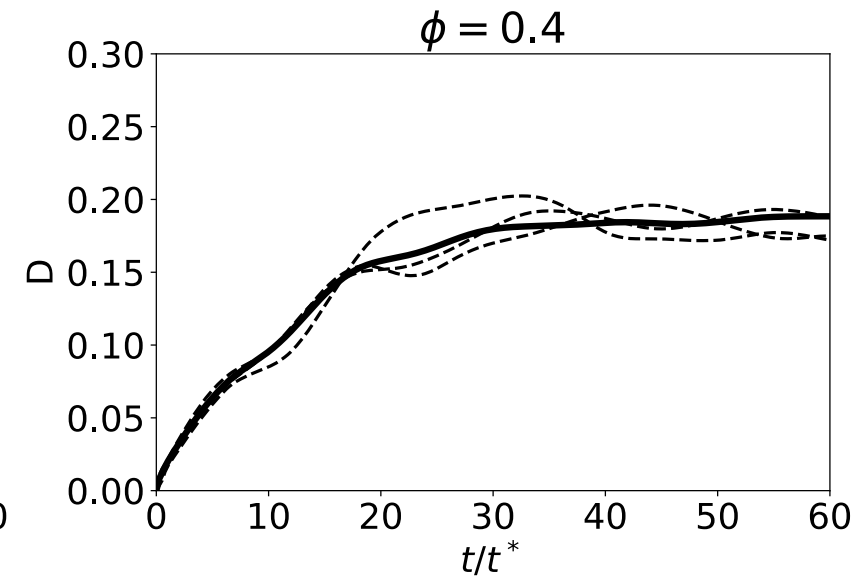
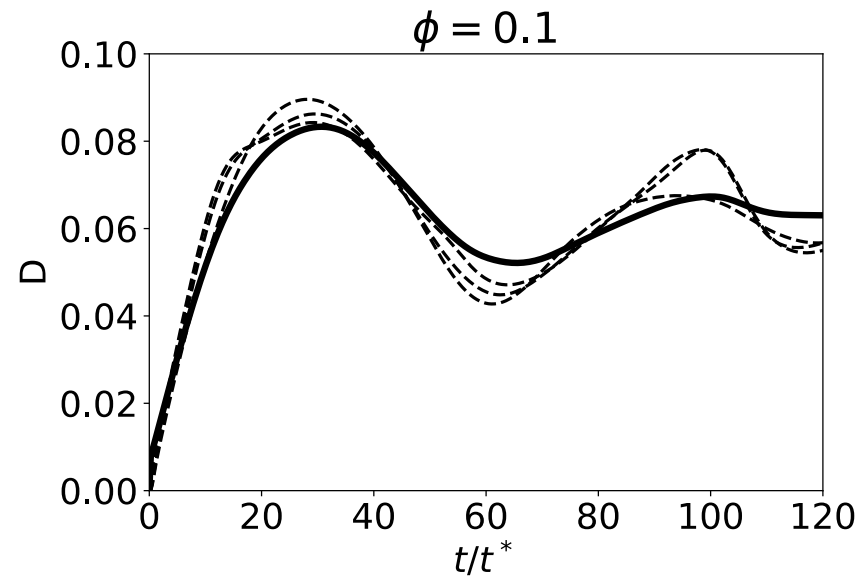
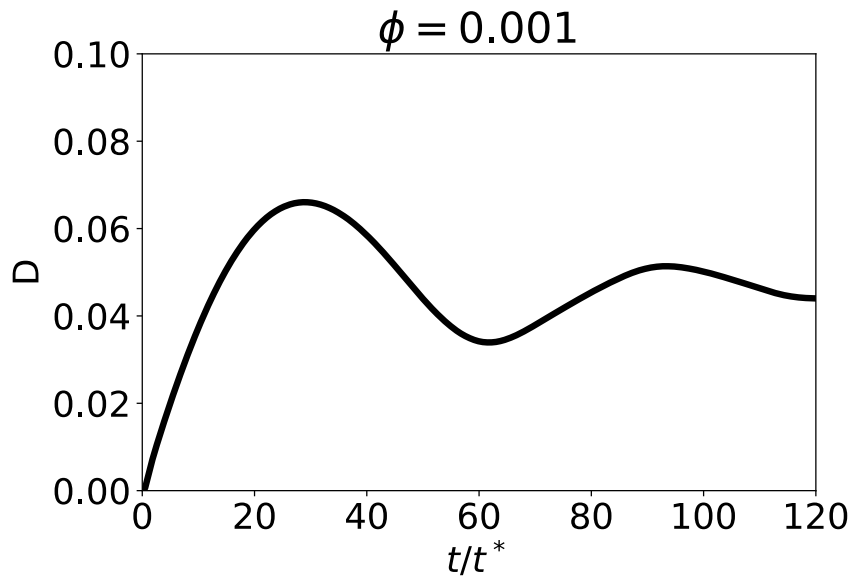
Loading time and frequency



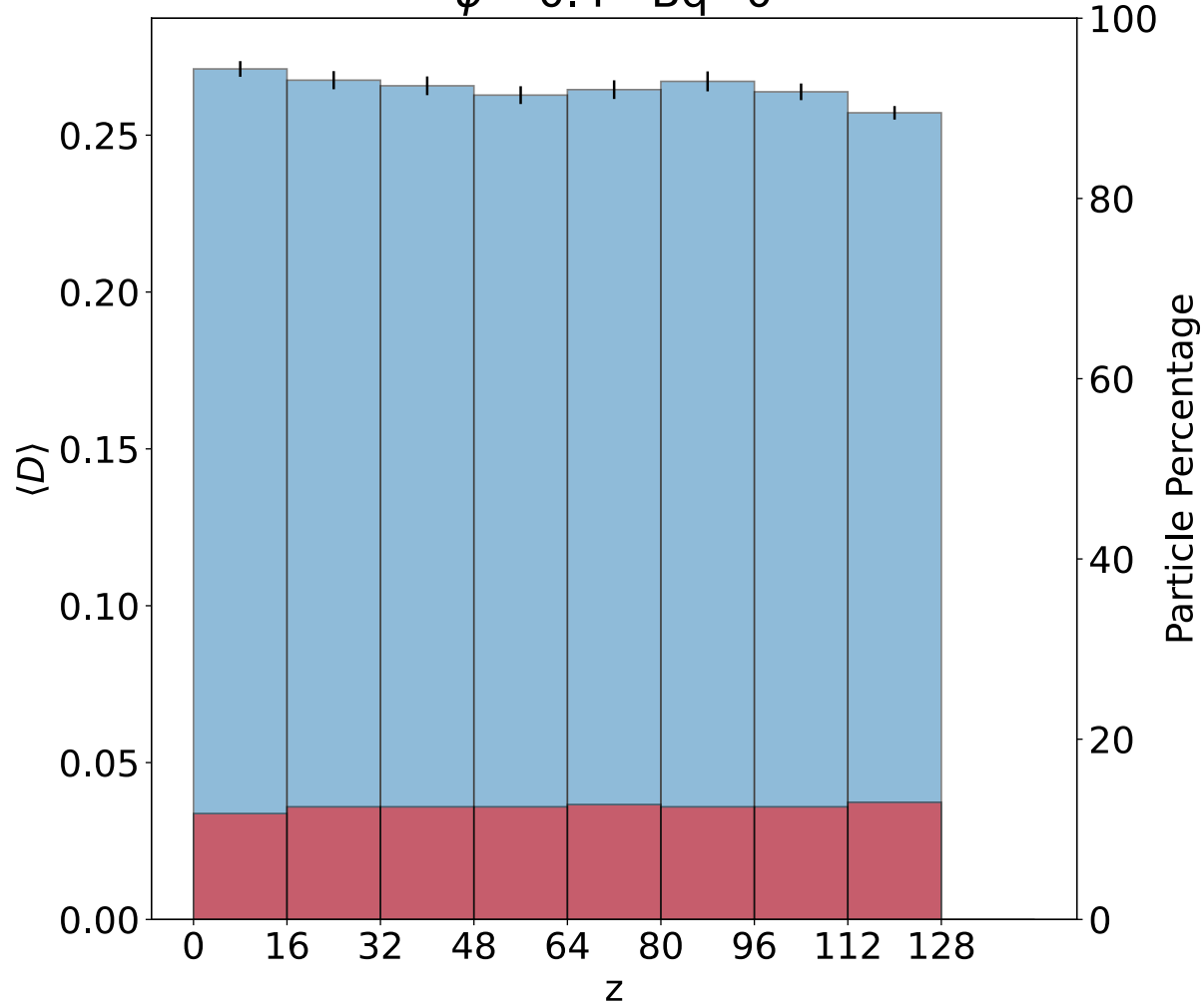
Single capsule: particle stress







$\phi = 0.4 - Bq=0$



$\phi = 0.4 - Bq=50$

